

# LMC6062 Precision CMOS Dual Micropower Operational Amplifier

Check for Samples: LMC6062

#### **FEATURES**

- (Typical Unless Otherwise Noted)
- Low Offset Voltage 100μV
- Ultra Low Supply current 16µA/Amplifier
- Operates from 4.5V to 15V Single Supply
- Ultra Low Input Bias Current 10fA
- Output Swing within 10mV of Supply Rail, 100k Load
- Input Common-Mode Range Includes V<sup>-</sup>
- High Voltage Gain 140dB
- Improved Latchup Immunity

#### **APPLICATIONS**

- Instrumentation Amplifier
- Photodiode and Infrared Detector Preamplifier
- Transducer Amplifiers
- Hand-Held Analytic Instruments
- Medical Instrumentation
- D/A Converter
- Charge Amplifier for Piezoelectric Transducers

## **Connection Diagram**

# 

Figure 1. 8-Pin PDIP/SOIC Top View

## DESCRIPTION

The LMC6062 is a precision dual low offset voltage, micropower operational amplifier, capable of precision single supply operation. Performance characteristics include ultra low input bias current, high voltage gain, rail-to-rail output swing, and an input common mode voltage range that includes ground. These features, plus its low power consumption, make the LMC6062 ideally suited for battery powered applications.

Other applications using the LMC6062 include precision full-wave rectifiers, integrators, references, sample-and-hold circuits, and true instrumentation amplifiers.

This device is built with TI's advanced double-Poly Silicon-Gate CMOS process.

For designs that require higher speed, see the LMC6082 precision dual operational amplifier.

#### **PATENT PENDING**

Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.





This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

## Absolute Maximum Ratings (1)(2)

Differential Input Voltage	±Supply Voltage
Voltage at Input/Output Pin	(V <sup>+</sup> ) +0.3V,
	(V <sup>-</sup> ) -0.3V
Supply Voltage (V <sup>+</sup> - V <sup>-</sup> )	16V
Output Short Circuit to V <sup>+</sup>	See (3)
Output Short Circuit to V	See (4)
Lead Temperature (Soldering, 10 sec.)	260°C
Storage Temp. Range	-65°C to +150°C
Junction Temperature	150°C
ESD Tolerance <sup>(5)</sup>	2 kV
Current at Input Pin	±10 mA
Current at Output Pin	±30 mA
Current at Power Supply Pin	40 mA
Power Dissipation	See (6)

- (1) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but do not ensure specific performance limits. For ensured specifications and test conditions, see the Electrical Characteristics. The ensured specifications apply only for the test conditions listed.
- (2) If Military/Aerospace specified devices are required, please contact the TI Sales Office/Distributors for availability and specifications
- (3) Do not connect output to V+, when V+ is greater than 13V or reliability witll be adversely affected.
- (4) Applies to both single-supply and split-supply operation. Continuos short circuit operation at elevated ambient temperature can result in exceeding the maximum allowed junction temperature of 150°C. Output currents in excess of ±30 mA over long term may adversely affect reliability.
- (5) Human body model, 1.5 kΩ in series with 100 pF.
- (6) The maximum power dissipation is a function of T<sub>J(Max)</sub>, θ<sub>JA</sub>, and T<sub>A</sub>. The maximum allowable power dissipation at any ambient temperature is P<sub>D</sub> = (T<sub>J(Max)</sub> T<sub>A</sub>)/θ<sub>JA</sub>.

## Operating Ratings (1)

Temperature Range	LMC6062AM	-55°C ≤ T <sub>J</sub> ≤ +125°C
	LMC6062AI, LMC6082I	-40°C ≤ T <sub>J</sub> ≤ +85°C
Supply Voltage		4.5V ≤ V <sup>+</sup> ≤ 15.5V
Thermal Resistance (θ <sub>JA</sub> ) (2)	8-Pin PDIP	115°C/W
	8-Pin SOIC	193°C/W
Power Dissipation		See (3)

- (1) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but do not ensure specific performance limits. For ensured specifications and test conditions, see the Electrical Characteristics. The ensured specifications apply only for the test conditions listed.
- (2) All numbers apply for packages soldered directly into a PC board.
- (3) For operating at elevated temperatures the device must be derated based on the thermal resistance  $\theta_{JA}$  with  $P_D = (T_J T_A)/\theta_{JA}$ .

## DC Electrical Characteristics(1)

Unless otherwise specified, all limits ensured for  $T_J = 25$ °C. **Boldface** limits apply at the temperature extremes.  $V^+ = 5V$ ,  $V^- = 0V$ ,  $V_{CM} = 1.5V$ ,  $V_O = 2.5V$  and  $R_L > 1M$  unless otherwise specified.

Symbol	Parameter	Conditions	Typ <sup>(2)</sup>	LMC6062AM Limit <sup>(3)</sup>	LMC6062AI Limit <sup>(3)</sup>	LMC6062I Limit <sup>(3)</sup>	Units
V <sub>OS</sub>	Input Offset Voltage		100	350	350	800	μV
				1200	900	1300	Max

- (1) For ensured Military Temperature Range parameters, see RETSMC6062X.
- (2) Typical values represent the most likely parametric norm.
- (3) All limits are ensured by testing or statistical analysis.



# DC Electrical Characteristics<sup>(1)</sup> (continued)

Unless otherwise specified, all limits ensured for  $T_J = 25^{\circ}C$ . **Boldface** limits apply at the temperature extremes.  $V^+ = 5V$ ,  $V^- = 0V$ ,  $V_{CM} = 1.5V$ ,  $V_O = 2.5V$  and  $R_L > 1M$  unless otherwise specified.

Symbol	Parameter	Condit	ions	Typ <sup>(2)</sup>	LMC6062AM Limit <sup>(3)</sup>	LMC6062AI Limit <sup>(3)</sup>	LMC6062I Limit <sup>(3)</sup>	Units
TCV <sub>OS</sub>	Input Offset Voltage Average Drift			1.0				μV/°C
I <sub>B</sub>	Input Bias Current			0.010				pA
					100	4	4	Max
los	Input Offset Current			0.005				pА
					100	2	2	Max
R <sub>IN</sub>	Input Resistance			>10				Tera Ω
CMRR	Common Mode	$0V \le V_{CM} \le 12.0$	V	85	75	75	66	dB
	Rejection Ratio	V <sup>+</sup> = 15V			70	72	63	Min
+PSRR	Positive Power Supply	5V ≤ V <sup>+</sup> ≤ 15V		85	75	75	66	dB
	Rejection Ratio	$V_O = 2.5V$			70	72	63	Min
-PSRR	Negative Power Supply	0V ≤ V <sup>-</sup> ≤ −10V		100	84	84	74	dB
	Rejection Ratio				70	81	71	Min
$V_{CM}$	Input Common-Mode	V <sup>+</sup> = 5V and 15\	V	-0.4	-0.1	-0.1	-0.1	V
	Voltage Range	for CMRR ≥ 60	dB		0	0	0	Max
				V <sup>+</sup> - 1.9	V <sup>+</sup> - 2.3	V <sup>+</sup> - 2.3	V <sup>+</sup> - 2.3	V
					V+ - 2.6	V+ - 2.5	V+ - 2.5	Min
A <sub>V</sub>	Large Signal	$R_L = 100 \text{ k}\Omega^{(4)}$	Sourcing	4000	400	400	300	V/mV
	Voltage Gain				200	300	200	Min
			Sinking	3000	180	180	90	V/mV
					70	100	60	Min
		$R_L = 25 k\Omega^{(4)}$	Sourcing	3000	400	400	200	V/mV
					150	150	80	Min
			Sinking	2000	100	100	70	V/mV
					35	50	35	Min
Vo	Output Swing	V <sup>+</sup> = 5V		4.995	4.990	4.990	4.950	V
		$R_L = 100 \text{ k}\Omega \text{ to } \Omega$	2.5V		4.970	4.980	4.925	Min
		_		0.005	0.010	0.010	0.050	V
					0.030	0.020	0.075	Max
		V <sup>+</sup> = 5V		4.990	4.975	4.975	4.950	V
		$R_L = 25 \text{ k}\Omega \text{ to } 2.$	.5V		4.955	4.965	4.850	Min
		_		0.010	0.020	0.020	0.050	V
					0.045	0.035	0.150	Max
		V <sup>+</sup> = 15V		14.990	14.975	14.975	14.950	V
		$R_L = 100 \text{ k}\Omega \text{ to } T$	7.5V		14.955	14.965	14.925	Min
				0.010	0.025	0.025	0.050	V
					0.050	0.035	0.075	Max
		V <sup>+</sup> = 15V		14.965	14.900	14.900	14.850	V
		$R_L = 25 \text{ k}\Omega \text{ to } 7.$	.5V		14.800	14.850	14.800	Min
			- •	0.025	0.050	0.050	0.100	V
					0.200	0.150	0.200	Max

(4)  $V^+ = 15V$ ,  $V_{CM} = 7.5V$  and  $R_L$  connected to 7.5V. For Sourcing tests,  $7.5V \le V_O \le 11.5V$ . For Sinking tests,  $2.5V \le V_O \le 7.5V$ .



## DC Electrical Characteristics<sup>(1)</sup> (continued)

Unless otherwise specified, all limits ensured for  $T_J = 25$ °C. **Boldface** limits apply at the temperature extremes.  $V^+ = 5V$ ,  $V^- = 5V$ 0V,  $V_{CM} = 1.5V$ ,  $V_{O} = 2.5V$  and  $R_{L} > 1M$  unless otherwise specified.

Symbol	Parameter	Conditions	Typ <sup>(2)</sup>	LMC6062AM Limit <sup>(3)</sup>	LMC6062AI Limit <sup>(3)</sup>	LMC6062I Limit <sup>(3)</sup>	Units
Io	Output Current	Sourcing, V <sub>O</sub> = 0V	22	16	16	13	mA
	V <sup>+</sup> = 5V			8	10	8	Min
		Sinking, V <sub>O</sub> = 5V	21	16	16	16	mA
				7	8	8	Min
Io	Output Current	Sourcing, V <sub>O</sub> = 0V	25	15	15	15	mA
	V <sup>+</sup> = 15V			9	10	10	Min
		Sinking, $V_O = 13V^{(5)}$	35	20	20	20	mA
				7	8	8	Min
Is	Supply Current	Both Amplifiers	32	38	38	46	μΑ
		$V^+ = +5V, V_O = 1.5V$		60	46	56	Max
		Both Amplifiers	40	47	47	57	μΑ
		$V^+ = +15V, V_O = 7.5V$		70	55	66	Max

<sup>(5)</sup> Do not connect output to V<sup>+</sup>, when V<sup>+</sup> is greater than 13V or reliability will be adversely affected.

### AC Electrical Characteristics(1)

Unless otherwise specified, all limits ensured for  $T_J = 25$ °C, **Boldface** limits apply at the temperature extremes.  $V^+ = 5V$ ,  $V^- = 5V$ 0V,  $V_{CM} = 1.5V$ ,  $V_{O} = 2.5V$  and  $R_{I} > 1M$  unless otherwise specified.

Symbol	Parameter	Conditions	Typ <sup>(2)</sup>	LMC6062AM Limit <sup>(3)</sup>	LMC6062AI Limit <sup>(3)</sup>	LMC6062I Limit <sup>(3)</sup>	Units
SR	Slew Rate	See (4)	35	20	20	15	V/ms
				8	10	7	Min
GBW	Gain-Bandwidth Product		100				kHz
$\theta_{m}$	Phase Margin		50				Deg
	Amp-to-Amp Isolation	See (5)	155				dB
e <sub>n</sub>	Input-Referred Voltage Noise	F = 1 kHz	83				nV/√ <del>Hz</del>
in	Input-Referred Current Noise	F = 1 kHz	0.0002				pA/√ <del>Hz</del>
T.H.D.	Total Harmonic Distortion	F = 1 kHz, A <sub>V</sub> = −5					
		$R_L = 100 \text{ k}\Omega, V_O = 2 V_{PP}$	0.01				%
ı		±5V Supply					

- For ensured Military Temperature Range parameters, see RETSMC6062X.
- Typical values represent the most likely parametric norm.
- All limits are ensured by testing or statistical analysis.  $V^+ = 15V$ . Connected as Voltage Follower with 10V step input. Number specified is the slower of the positive and negative slew rates. Input referred  $V^+ = 15V$  and  $R_L = 100 \text{ k}\Omega$  connected to 7.5V. Each amp excited in turn with 100 Hz to produce  $V_O = 12 \text{ V}_{PP}$ .

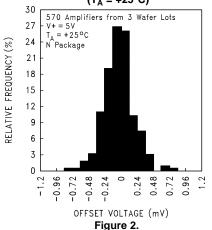
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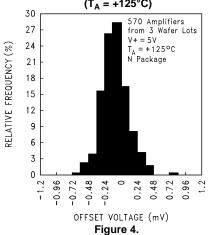
## **Typical Performance Characteristics**

 $V_S = \pm 7.5V$ ,  $T_A = 25$ °C, Unless otherwise specified

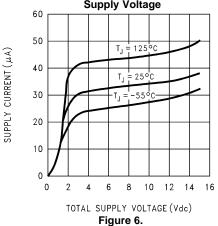
# Distribution of LMC6062 Input Offset Voltage (T<sub>A</sub> = +25°C)



# Distribution of LMC6062 Input Offset Voltage (T<sub>A</sub> = +125°C)



## **Supply Current** vs. Supply Voltage



# Distribution of LMC6062 Input Offset Voltage $(T_A = -55^{\circ}C)$

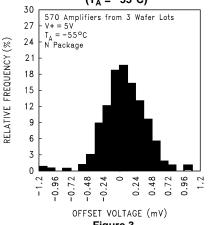


Figure 3.

#### **Input Bias Current**

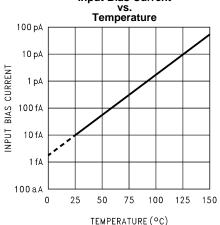


Figure 5.

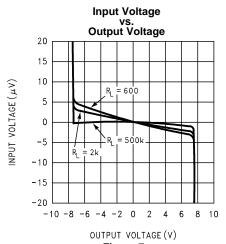


Figure 7.

VOLTAGE NOISE (nV//Hz)

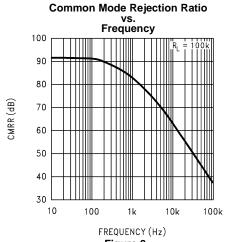
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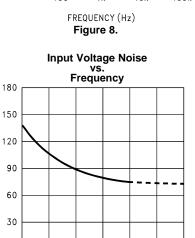
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## **Typical Performance Characteristics (continued)**

 $V_S = \pm 7.5V$ ,  $T_A = 25$ °C, Unless otherwise specified

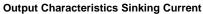


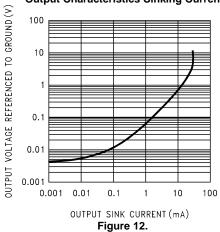


FREQUENCY (Hz) Figure 10.

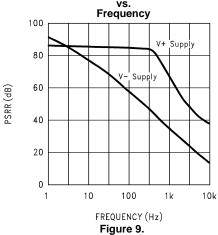
10k

100





Power Supply Rejection Ratio vs. Frequency



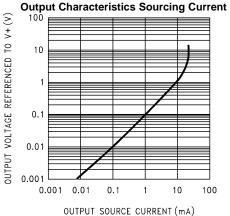


Figure 11.

#### **Gain and Phase Response**

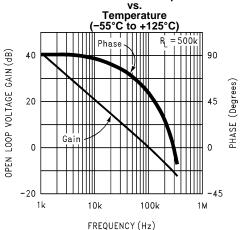


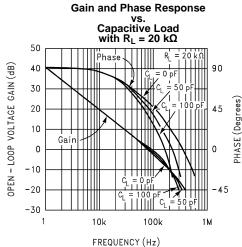
Figure 13.

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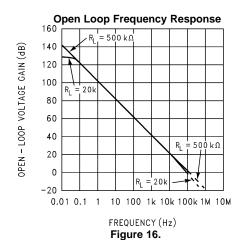


## **Typical Performance Characteristics (continued)**

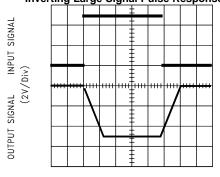
 $V_S = \pm 7.5V$ ,  $T_A = 25$ °C, Unless otherwise specified







**Inverting Large Signal Pulse Response** 



TIME (100  $\mu$ s/Div) **Figure 18.** 

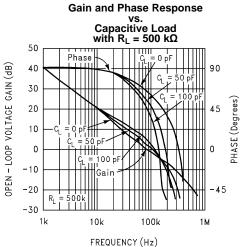
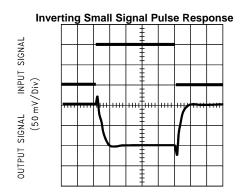
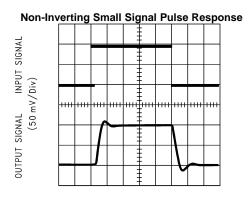


Figure 15.



TIME (10  $\mu$ s/Div)

Figure 17.



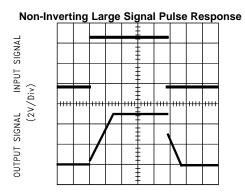
TIME (10 μs/Div)

Figure 19.



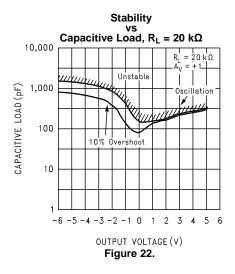
## **Typical Performance Characteristics (continued)**

 $V_S = \pm 7.5V$ ,  $T_A = 25$ °C, Unless otherwise specified



TIME (100 μs/Div)





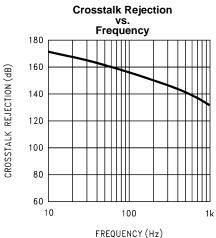
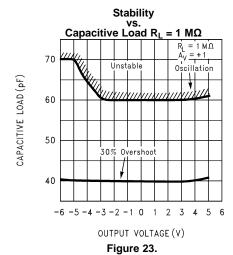


Figure 21.



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#### APPLICATIONS HINTS

#### **AMPLIFIER TOPOLOGY**

The LMC6062 incorporates a novel op-amp design topology that enables it to maintain rail-to-rail output swing even when driving a large load. Instead of relying on a push-pull unity gain output buffer stage, the output stage is taken directly from the internal integrator, which provides both low output impedance and large gain. Special feed forward compensation design techniques are incorporated to maintain stability over a wider range of operating conditions than traditional micropower op amps. These features make the LMC6062 both easier to design with, and provide higher speed than products typically found in this ultra low power class.

#### COMPENSATING FOR INPUT CAPACITANCE

It is quite common to use large values of feedback resistance for amplifiers with ultra-low input current, like the LMC6062.

Although the LMC6062 is highly stable over a wide range of operating conditions, certain precautions must be met to achieve the desired pulse response when a large feedback resistor is used. Large feedback resistors and even small values of input capacitance, due to transducers, photodiodes, and circuit board parasitics, reduce phase margins.

When high input impedances are demanded, guarding of the LMC6062 is suggested. Guarding input lines will not only reduce leakage, but lowers stray input capacitance as well. (See PRINTED-CIRCUIT-BOARD LAYOUT FOR HIGH-IMPEDANCE WORK).

The effect of input capacitance can be compensated for by adding a capacitor. Place a capacitor,  $C_f$ , around the feedback resistor (as in Figure 24) such that:

$$\frac{1}{2\pi R_1 C_{\text{IN}}} \ge \frac{1}{2\pi R_2 C_{\text{f}}} \tag{1}$$

or

$$R_1 C_{IN} \le R_2 C_f \tag{2}$$

Since it is often difficult to know the exact value of  $C_{IN}$ ,  $C_f$  can be experimentally adjusted so that the desired pulse response is achieved. Refer to the LMC660 and the LMC662 for a more detailed discussion on compensating for input capacitance.

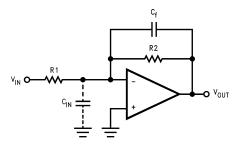


Figure 24. Canceling the Effect of Input Capacitance

#### **CAPACITIVE LOAD TOLERANCE**

All rail-to-rail output swing operational amplifiers have voltage gain in the output stage. A compensation capacitor is normally included in this integrator stage. The frequency location of the dominate pole is affected by the resistive load on the amplifier. Capacitive load driving capability can be optimized by using an appropriate resistive load in parallel with the capacitive load (see typical curves).

Direct capacitive loading will reduce the phase margin of many op-amps. A pole in the feedback loop is created by the combination of the op-amp's output impedance and the capacitive load. This pole induces phase lag at the unity-gain crossover frequency of the amplifier resulting in either an oscillatory or underdamped pulse response. With a few external components, op amps can easily indirectly drive capacitive loads, as shown in Figure 25.



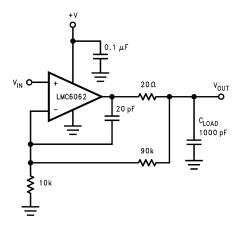


Figure 25. LMC6062 Noninverting Gain of 10 Amplifier, Compensated to Handle Capacitive Loads

In the circuit of Figure 25, R1 and C1 serve to counteract the loss of phase margin by feeding the high frequency component of the output signal back to the amplifier's inverting input, thereby preserving phase margin in the overall feedback loop.

Capacitive load driving capability is enhanced by using a pull up resistor to V $^+$  (Figure 26). Typically a pull up resistor conducting 10  $\mu$ A or more will significantly improve capacitive load responses. The value of the pull up resistor must be determined based on the current sinking capability of the amplifier with respect to the desired output swing. Open loop gain of the amplifier can also be affected by the pull up resistor (see Electrical Characteristics).

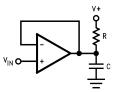


Figure 26. Compensating for Large Capacitive Loads with a Pull Up Resistor

#### PRINTED-CIRCUIT-BOARD LAYOUT FOR HIGH-IMPEDANCE WORK

It is generally recognized that any circuit which must operate with less than 1000 pA of leakage current requires special layout of the PC board. When one wishes to take advantage of the ultra-low bias current of the LMC6062, typically less than 10 fA, it is essential to have an excellent layout. Fortunately, the techniques of obtaining low leakages are quite simple. First, the user must not ignore the surface leakage of the PC board, even though it may sometimes appear acceptably low, because under conditions of high humidity or dust or contamination, the surface leakage will be appreciable.

To minimize the effect of any surface leakage, lay out a ring of foil completely surrounding the LMC6062's inputs and the terminals of capacitors, diodes, conductors, resistors, relay terminals etc. connected to the op-amp's inputs, as in Figure 27. To have a significant effect, guard rings should be placed on both the top and bottom of the PC board. This PC foil must then be connected to a voltage which is at the same voltage as the amplifier inputs, since no leakage current can flow between two points at the same potential. For example, a PC board trace-to-pad resistance of  $10^{12}\Omega$ , which is normally considered a very large resistance, could leak 5 pA if the trace were a 5V bus adjacent to the pad of the input. This would cause a 100 times degradation from the LMC6062's actual performance. However, if a guard ring is held within 5 mV of the inputs, then even a resistance of  $10^{11}\Omega$  would cause only 0.05 pA of leakage current. See Figure 28 for typical connections of guard rings for standard op-amp configurations.



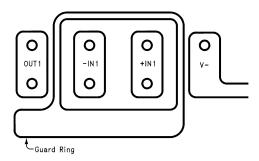


Figure 27. Example of Guard Ring in P.C. Board Layout

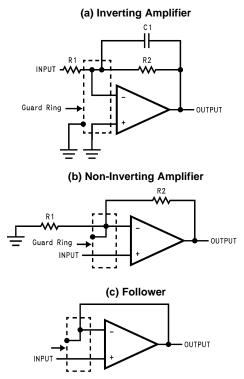


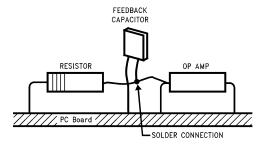
Figure 28. Typical Connections of Guard Rings

The designer should be aware that when it is inappropriate to lay out a PC board for the sake of just a few circuits, there is another technique which is even better than a guard ring on a PC board: Don't insert the amplifier's input pin into the board at all, but bend it up in the air and use only air as an insulator. Air is an excellent insulator. In this case you may have to forego some of the advantages of PC board construction, but the advantages are sometimes well worth the effort of using point-to-point up-in-the-air wiring. See Figure 29.

#### Latchup

CMOS devices tend to be susceptible to latchup due to their internal parasitic SCR effects. The (I/O) input and output pins look similar to the gate of the SCR. There is a minimum current required to trigger the SCR gate lead. The LMC6062 and LMC6082 are designed to withstand 100 mA surge current on the I/O pins. Some resistive method should be used to isolate any capacitance from supplying excess current to the I/O pins. In addition, like an SCR, there is a minimum holding current for any latchup mode. Limiting current to the supply pins will also inhibit latchup susceptibility.





(Input pins are lifted out of PC board and soldered directly to components. All other pins connected to PC board).

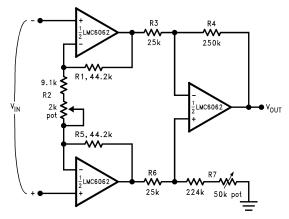
Figure 29. Air Wiring

### **Typical Single-Supply Applications**

$$(V^+ = 5.0 V_{DC})$$

The extremely high input impedance, and low power consumption, of the LMC6062 make it ideal for applications that require battery-powered instrumentation amplifiers. Examples of these types of applications are hand-held pH probes, analytic medical instruments, magnetic field detectors, gas detectors, and silicon based pressure transducers.

Figure 30 shows an instrumentation amplifier that features high differential and common mode input resistance (>10<sup>14</sup> $\Omega$ ), 0.01% gain accuracy at A<sub>V</sub> = 100, excellent CMRR with 1 k $\Omega$  imbalance in bridge source resistance. Input current is less than 100 fA and offset drift is less than 2.5  $\mu$ V/°C. R<sub>2</sub> provides a simple means of adjusting gain over a wide range without degrading CMRR. R<sub>7</sub> is an initial trim used to maximize CMRR without using super precision matched resistors. For good CMRR over temperature, low drift resistors should be used.



If  $R_1 = R_5$ ,  $R_3 = R_6$ , and  $R_4 = R_7$ ; then

$$\frac{V_{OUT}}{V_{IN}} = \frac{R_2\,+\,2R_1}{R_2} \times \frac{R_4}{R_3}$$

∴ $A_V$  ≈ 100 for circuit shown ( $R_2$  = 9.822k).

Figure 30. Instrumentation Amplifier



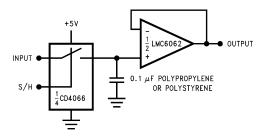


Figure 31. Low-Leakage Sample and Hold

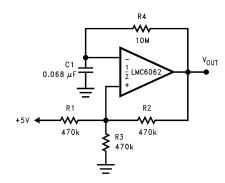


Figure 32. 1 Hz Square Wave Oscillator

### SNOS631D-NOVEMBER 1994-REVISED MARCH 2013



## **REVISION HISTORY**

Cł	Changes from Revision C (March 2013) to Revision D			
•	Changed layout of National Data Sheet to TI format		13	





19-Mar-2015

#### PACKAGING INFORMATION

Orderable Device	Status	Package Type	Package Drawing	Pins	Package Qty	Eco Plan	Lead/Ball Finish	MSL Peak Temp	Op Temp (°C)	Device Marking (4/5)	Samples
LMC6062AIM	NRND	SOIC	D	8	95	TBD	Call TI	Call TI	-40 to 85	LMC60 62AIM	
LMC6062AIM/NOPB	ACTIVE	SOIC	D	8	95	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 85	LMC60 62AIM	Samples
LMC6062AIMX/NOPB	ACTIVE	SOIC	D	8	2500	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 85	LMC60 62AIM	Samples
LMC6062IM	NRND	SOIC	D	8	95	TBD	Call TI	Call TI	-40 to 85	LMC60 62IM	
LMC6062IM/NOPB	ACTIVE	SOIC	D	8	95	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 85	LMC60 62IM	Samples
LMC6062IMX	NRND	SOIC	D	8	2500	TBD	Call TI	Call TI	-40 to 85	LMC60 62IM	
LMC6062IMX/NOPB	ACTIVE	SOIC	D	8	2500	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 85	LMC60 62IM	Samples
LMC6062IN/NOPB	ACTIVE	PDIP	Р	8	40	Green (RoHS & no Sb/Br)	CU SN	Level-1-NA-UNLIM	-40 to 85	LMC6062 IN	Samples

<sup>(1)</sup> The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

TBD: The Pb-Free/Green conversion plan has not been defined.

**Pb-Free** (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes. **Pb-Free** (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

<sup>(2)</sup> Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

<sup>(3)</sup> MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.



## PACKAGE OPTION ADDENDUM

19-Mar-2015

- (4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.
- (5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
- (6) Lead/Ball Finish Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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## PACKAGE MATERIALS INFORMATION

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## TAPE AND REEL INFORMATION





-	Α0	Dimension designed to accommodate the component width
		Dimension designed to accommodate the component length
	K0	Dimension designed to accommodate the component thickness
		Overall width of the carrier tape
-	P1	Pitch between successive cavity centers

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



#### \*All dimensions are nominal

Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
LMC6062AIMX/NOPB	SOIC	D	8	2500	330.0	12.4	6.5	5.4	2.0	8.0	12.0	Q1
LMC6062IMX	SOIC	D	8	2500	330.0	12.4	6.5	5.4	2.0	8.0	12.0	Q1
LMC6062IMX/NOPB	SOIC	D	8	2500	330.0	12.4	6.5	5.4	2.0	8.0	12.0	Q1

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\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
LMC6062AIMX/NOPB	SOIC	D	8	2500	367.0	367.0	35.0
LMC6062IMX	SOIC	D	8	2500	367.0	367.0	35.0
LMC6062IMX/NOPB	SOIC	D	8	2500	367.0	367.0	35.0

# P (R-PDIP-T8)

## PLASTIC DUAL-IN-LINE PACKAGE



NOTES:

- A. All linear dimensions are in inches (millimeters).
- B. This drawing is subject to change without notice.
- C. Falls within JEDEC MS-001 variation BA.



# D (R-PDSO-G8)

## PLASTIC SMALL OUTLINE



NOTES:

- A. All linear dimensions are in inches (millimeters).
- B. This drawing is subject to change without notice.
- Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.006 (0,15) each side.
- Body width does not include interlead flash. Interlead flash shall not exceed 0.017 (0,43) each side.
- E. Reference JEDEC MS-012 variation AA.



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